

Multiple Criteria Method for Designing Distillation Sequence for Sharp Separation

A.G. Kamel¹, M.Kaoud² and S.M. Aly³

^{1,2,3} Department of Chemical and Refining Engineering, Suez University, Egypt.

ORCID: 0000-0002-4320-3778 (Kaoud)

Abstract

In almost every chemical process, distillation depending on sequences of separation. These systems of separation are utilized for preparation of feed, for the separation of products and finishing as well as for the waste treatment. This paper presents Multiple Criteria Approach for the synthesis of flow sheets with simple, sharp separator splitting. This approach based on quantification three heuristic rules will be used for selection of optimum separation sequence. The suggested procedure combines the values of the difference in normal boiling points of the components and the estimate separation mass load coefficients and relative volatility. The proposed method used to deal with previously reported literary problems produced optimal solutions which are better or at least similar to the optimum flow sheet with the indicated values, and overcame some obstacles of using the evolutionary, heuristic and mathematical programming. The proposed algorithm can be implement by hand calculation and characterized by its simplicity.

Keywords: Process synthesis; sharp separation; multiple criteria separation.

1. INTRODUCTION

One of the most important subjects in process synthesis has been the synthesis of optimum sequences of separation. Separation processes represent a significant portion of the operating expenses and the chemical plant's total capital investment, and a great deal of interest has been generated in developing systematic approaches that will select optimum sequences of separation much interest has been developed in developing systematic approaches that will select optimum sequences of separation. In the chemical unit design of sharp separation sequence is consider one of the most examined problems.

For the synthesis of sharp separation sequence Several of published works that have dealt with the synthesis, the main papers are reviewed in this area in Hendry et al.[1],Hlavacked [2],Westerberg [3],Stephanopolous [4],Nishida et al. [5],Umeda[6],Westerberger [7] and Floquet et al [8]. These authors proposed the following method, for resolving sharp

separator sequence synthesis which could be categorizes into (3) key categories:-

Algorithmic methods attempt to solve and optimize the problem through the use of algorithms developed in the field of discrete mathematical programming, the major procedures used in the literature are the following:-

- 1- Dynamic programming (Hendry and Hughes [9].
- 2- Branch and bound type method (Westerberg and Stephanopoulos [10]; Rodrigo and seader [11].
- 3- Mixed integer linear programming methods (Andreacovich and Westerberg [12]; Floquet et al [13]

Evolutionary strategies attempt to identify the better scheme of separation by a sequence of evolutionary enhancements. The evolutionary approach depends on both the initial flow sheet and the evolutionary strategies, which can be categorizes into (2) key categories Heuristic strategy (Nath and Motard [14];Lu and Motard [15];Breadth first or depth first strategies (Stephanopoulos and Westerberg [16]; seader and Westerberg [17] Heuristic methods user rules of thumb resulting from long experience (Heaven [18];Powers [19];Nishimura et Hiraizumi[20]; Thompson and king [21];rudd et al. [22];NiIda et al.[23]; Dougls [24]. In this paper a synthesis approach suggested for sharp separation sequences combining the quantification three rules ,difference in normal boiling point of components and relative volatility and the values of estimate separation mass load coefficient in multiple criteria decision method The effectiveness of this synthesis approach is illustrated using two problems.

2. PROBLEM STATEMENT

In the synthesis of chemical units. The design of sharp separation sequences is consider one of the most studied problems it could be stating as follows:

In the context a single multicomponent feed mixture with known conditions (i.e. flow rate, composition, pressure and temperature) synthesize a process which can separate the wanted products from the feed at minimum annual cost (including the sum of the plant's annual operating costs and investment costs).

3. SOLUTION METHOD

The suggested methods for resolving synthesis of sharp separator sequence can be categorized into (3) key categories:

Evolutionary strategies, heuristic methods and Algorithmic methods

The procedure described below is in the heuristic range and allows flow sheet structures to be easily found which are also nearly ideal solutions.

3.1 Quantification of the Rules

The synthesis algorithm is based on the application of expert rules, well suited for economical design problem. From an extensive compilation of three rules of thumb have been retained:

- I. If the difference ΔT_b of the normal boiling point temperatures between two adjacent key components is big then split between these two components.
- II. Favor the separation at the point where the relative volatility $\alpha_{i,j}$ of two adjacent key components is the most important.
- III. When the value of the estimated mass load (EML) coefficient of the split is small, perform this split.

Rule 1:

$$\mu^1 = \left\{ \begin{array}{ll} 0 & \dots\dots\dots \text{if } \Delta T_b \leq T_{\min} \\ \frac{\Delta T_b - T_{\min}}{T_{\max} - T_{\min}} & \dots\dots \text{if } T_{\min} \leq \Delta T_b \leq T_{\max} \\ 1 & \dots\dots\dots \text{if } \Delta T_b \geq T_{\max} \end{array} \right\} \dots\dots(1)$$

With $T_{\min} = \min(\Delta T_b)$ and $T_{\max} = \sum_{j=1}^{n-1} \Delta T_b / (n-1)$

Rule 2:

$$\mu^2 = \left\{ \begin{array}{ll} 0 & \dots\dots \text{if } \alpha_{i,j} \leq 1.1 \\ (\alpha_{i,j} - 1.1) / 0.9 & \dots\dots \text{if } 1.1 \leq \alpha_{i,j} \leq 2 \\ 1 & \dots\dots \text{if } \alpha_{i,j} > 2 \end{array} \right\} \dots\dots(2)$$

Rule 3:

$$\mu^3 = \left\{ \begin{array}{ll} 0 & \dots\dots \text{if } EML < EML_{\min} \\ \frac{EML_{\max} - EML}{EML_{\max} - EML_{\min}} & \dots \text{if } EML_{\min} \leq EML \leq EML_{\max} \\ 1 & \dots\dots \text{if } EML > EML_{\max} \end{array} \right\} \dots\dots(3)$$

Estimated Mass Load (EML) coefficients definition and calculation The (EML) coefficients define as The molar flow rate which all separation units have to process downstream of the current separator before isolation of all the products required (Lu and Motard [25]).

Without make reference to the physical properties of the components, the numerical value of (EML) coefficients is the weighted likelihood of every possible downstream sequence. In the following table (where x_i is the molar fraction of the component I in the mixture), the main results are listed:

Table 1. Summary of the result of EML for N component

Number of component	EML Coefficients
1	0
2	$X_A + X_B = 1$
3	$3/2X_A + 2X_B + 3/2X_C$
4	$11/6X_A + 5/2X_B + 5/2X_C + 11/6X_D$
5	$25/12X_A + 17/6X_B + 3X_C + 17/6X_D + 25/12X_E$
N	$\sum_{i=1}^n a_{n,i} \text{ With } a_{1,1} = 0$ $a_{1,i} = \sum_{k=1}^{i-1} \frac{1}{k} \text{ if } i > 1$ $a_{1,i} = \sum_{k=1}^{i-1} \frac{1}{k} \text{ if } i > 1 + a_{1,i}$

The value of EML coefficient for a split is bounded; Table 2 showing these two boundaries for some splits.

$$EML_{\min} \leq EML \leq EML_{\max}$$

Table 2: Bounds on Estimated Mass Load (EML) coefficients for N=5 components

Splits	EML	EML min	EML max
A/BCDE	$O + 11/6X_B + 5/2X_C + 5/2X_D + 11/6X_E$	0	5/2
AB/CDE	$X_A + X_B + 3/2X_C + 2X_D + 3/2X_E$	1	2
ADC/DE	$3/2X_A + 2X_B + 3/2X_C + X_D + X_E$	1	2
ABCD/E	$11/6X_A + 5/2X_B + 5/2X_C + 11/6X_D + 0$	0	5/2
A/BCD or B/CDE	$O + 3/2X_B + 2X_C + 3/2X_D$	0	2
AB/CD or BC/DE	$X_A + X_B + X_C + X_D$	1	1
ABC/D or BCD/E	$3/2X_A + 2X_B + 3/2X_C + O$	0	2
A/BC	$O + X_B + X_C$	0	1
AB/C	$X_A + X_B + O$	0	1
A/B or B/C or C/D or D/E	0	0	0

3.2. Multiple criteria decision method

The multicriteria problem in its general form for a finite set A of n alternatives and certain system of m assessment criteria f_j , can be defined as following: (Diakoulaki, et.al. (26)

$$\text{Max } \{ f_1(a), f_2(a), \dots, f_m(a) / a \in A \} \dots \dots \dots (4)$$

We can define the membership function x_j For each criterion f_j of this multicriteria problem by layout the values of f_j to the interval [0,1]. This conversion is based on the ideal of the perfect point. Thus, the value x_{aj} below, expresses the degree to whichever the substitute is near to the ideal value f_j^* .whichever is the better performance in criterion j , and far from the anti-ideal value f_{j*} , which is the worse performance in criterion j both f_j^* and f_{j*} , are actualized by at the least one of the substitutes under consideration.

$$x_{aj} = [f_j(a) - f_{j*}] / [f_j^* - f_{j*}] \dots \dots \dots (5)$$

In this way the initial evaluation matrix is transformed into a matrix of relative scores with generic dimension x_{ij} . By examine the j th criterion in isolation, we generate a vector x_j showing the scores of all n substitutes considered.

$$x_j = (x_j(1), x_j(2), \dots, x_j(n)) \dots \dots \dots (6)$$

The standard deviation σ_j , which determines the contrast intensity of the corresponding criterion, is used for characterized each vector x_j . The standard deviation of x_j is also an indicator of its importance for decision-making. Instead of use of standard deviation it is apparent that any other of the divergency in scores could be used

$$\sigma_x = \sqrt{\frac{\sum_{i=1}^n (x_i - \bar{x})^2}{n-1}} \dots \dots \dots (7)$$

Where \bar{x} the mean variable of x and n is number of variable

The linear correlation coefficient R_{IK} between x_i and x_k is calculated

$$R_{IK} = \frac{n \sum x_i x_k - \sum x_i \sum x_k}{\sqrt{(n \sum x_i^2 - (\sum x_i)^2) \cdot (n \sum x_k^2 - (\sum x_k)^2)}} \dots \dots \dots (8)$$

The amount of C_j information emitted by the j th criterion can be identified

by composing measures that quantify the two notions by means of the following formula of multiplicative aggregation:-

$$C_j = \sigma_j \cdot \sum_{k=1}^m (1 - r_{jk}) \dots \dots \dots (9)$$

As per to the former analysis the higher the C_j value, the greater the amount of information given by the corresponding criterion and its relative relevance to the decision-making process is increased. Objective weights result from the normalization of those values to the unit in accordance with the equation below.

$$W_j = C_j / \sum_{k=1}^m C_k \dots \dots \dots (10)$$

Construct a multi - criteria ranking of the firms examined according to the following aggregation formula:

$$D_i = \sum_{j=1}^m W_j \cdot x_{ij} \dots \dots \dots (11)$$

Where:

D_i = the multicriteria score of firm i,

X_{ij} = the score of firm i under criterion j,

w_j = the weight criterion j

The strategy suggested is based on an assessment of the validity of each rule for every possible split. After the quantification step, the values of μ_1 , μ_2 and μ_3 for each split I are calculated and then multiple criteria decision method are applied.

Summarized of The key steps in the strategy showing in the following Fig.1

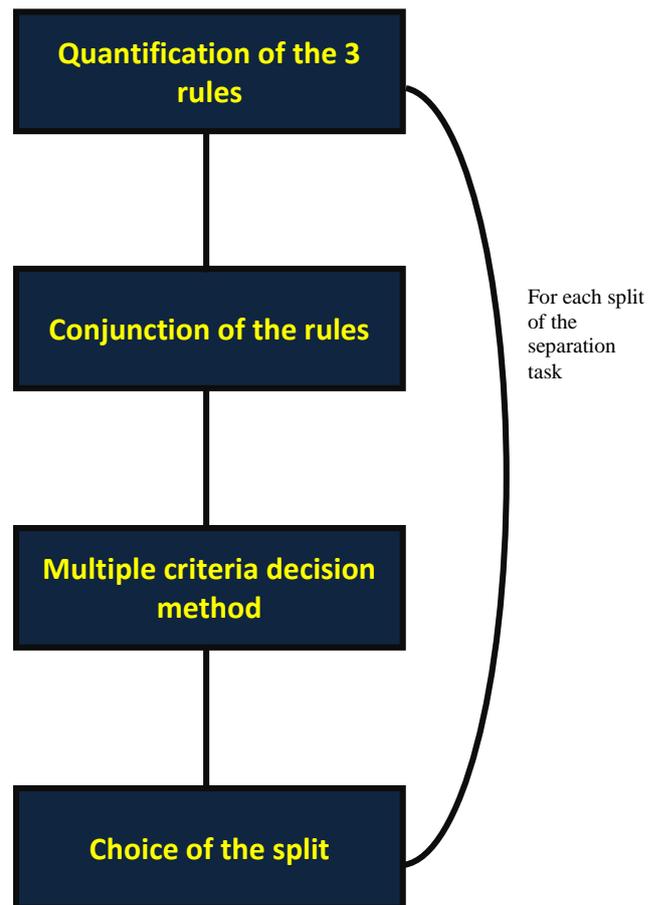


Fig.1 Main steps of the strategy

4. CASES STUDY

Example 1: Separation of a 4 component mixture

Consider the separation of the mixture of four light hydrocarbons into pure components by ordinary distillation Floudas And Anastasiadis [27] Studied this case the problem specification are given in Table 1

Table 3. Data of The problem specification

Component	Mole fraction	Boiling point temperature (k)	Normal boiling point difference (k)	Relative Volatility (α)
A:1-Butane	0.158	261.3		
			11.4	1.33
B:N-Butane	0.263	272.7		
			28.3	2.40
C:I-Pentane	0.210	300.8		
			8.20	1.52
D:N-Pentane	0.369	309		

The first step is to determine the boiling point difference and normalized and hence the corresponding estimated mass load values for every split by using equation 1, 2 and 3 Summarized of the calculations is showing in

Table 4. Summary of result by quantification of rules

Split	Boiling point Difference (ΔT_B)	Relative volatility (α)	Estimated mass load (EML)	Normalize boiling point difference (μ_1)	Normalize relative volatility (μ_2)	Normalize Estimated mass load (μ_3)
A/BCD	11.4	1.33	1.368	0.159	0	0.316
AB/CD	28.3	2.4	1	1	1	1
ABC/D	8.2	1.52	1.078	0	0.178	0.461

In the second step calculate the standard deviation for each parameter by using equation (7) is summary of the calculations is shown in table 3

Table 5. Summary of result for standard deviation

	A/BCD	AB/CD	ABC/D	Standard deviation (σ)
Normalize boiling point difference (μ_1)	0.159	1	0	0.53764
Normalize relative volatility (μ_2)	0	1	0.178	0.5334
Normalize Estimated mass load (μ_3)	0.316	1	0.461	0.360417

Then calculate the correlation R_{ik} between each two normalization variables by using equation (8).The values of R_{ik} are as follows: $R_{12}= 0.95$, $R_{13}= 0.939$ and $R_{23}= 0.999$

Applying equation (9) to get the quantity of information C_j emitted by the j^{th} criterion

Table 6. Summary of the results for standard deviation and C_j

spilt	Standard deviation (σ)	C_j
A/BCD	0.53764	0.059395
AB/CD	0.5334	0.026755
ABC/D	0.36041	0.022197

Applying equation (10) to obtain the object weight of each variable. The result as the following $W1 = 0.548317$, $W2 = 0.246866$ and $W3 = 0.204817$

For obtaining decision - maker, D, (or the multicriteria-score of firm), the following table is constructed:

Table 7. Evaluation of decision maker

Solution	$W1. \mu_1$	$W2. \mu_2$	$W3. \mu_3$	multi-criteria-score (D)	Ranking of firm
A/BCD	0.087182	0	0.064722	0.151904	2
AB/CD	0.548317	0.246866	0.204817	1	1
ABC/D	0	0.043942	0.09442	0.138363	3

By comparing the values of multicriteria-score (D) for all the possible split, split AB/CD is chosen for it yield the highest D value that is 1.

The resulting sequence is **AB/CD, A/B and C/D**

The cost of all possible towers is calculated by shortcut method and is shown in the following table 8

Table 8

Column	Cost*10 ⁵ (\$/yr.)	Column	Cost*10 ⁵ (\$/yr.)
A/BCD	7.200	C/D	6.922
AB/CD	5.869	B/C	2.099
ABC/D	10.801	A/B	3.345
B/CD	4.670	A/BC	6.400
BC/D	9.728	AB/C	3.778

The total cost of the possible separation sequences schemes as shown in table 9 is calculated by shortcut method, and it was found that the optimum sequence is consistent with the results of proposed method.

Table 9. The total cost of possible separation sequences schemes.

NO.	Separation	Cost*10 ⁵ (\$/yr.)
1	AB/CD, A/B, C/D	1.548
2	ABC/D, AB/C, A/B	1.792
3	A/BCD, B/CD, C/D	1.879
4	A/BCD, BC/D, B/C	1.903
5	ABC/D, A/BC, B/C	1.931

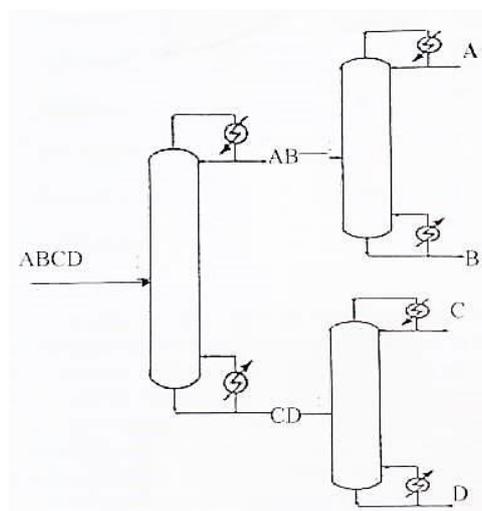


Fig.2 Optimum sequence for four-component mixture separation

Example 2:

The problem data are shown in table studied by Heaven [28] for separation the mixture of five light hydrocarbons into pure components by ordinary distillation

Table 10. Data for example 2:

Component	Mole fraction	Boiling point Temp (k)	Normal boiling Pt difference (k)	Relative volatility α
A: Propane	0.05	231.1		
			30.2	2.00
B: I-Butane	0.15	261.3		
			11.4	1.33
C: N-Butane	0.25	272.7		
			28.1	2.40
D: I-Pentane	0.2	300.8		
			8.2	1.52
E: N-Pentane	0.35	309.0		

The Summary of quantification rule is shown in the Table11:

Split	Boiling point Difference (ΔT_B)	Relative volatility (α)	Estimated mass load (EML)	Normalize boiling point difference (μ_1)	Normalize relative volatility (μ_2)	Normalize Estimated mass load (μ_3)
A/BCDE	30.2	2	2.042	1	1	0.1832
AB/CDE	11.4	1.33	1.5	0.145	0	0.5
ABC/DE	28.1	2.40	1.3	0.904	1	0.7
ABCD/E	8.2	1.52	1.458	0	0.178	0.416

The following table is summarized standard the calculation of standard deviation (σ) by equation (7) and amount of information (C_j) as shown in table 12

	A/BCDE	AB/CDE	AB/CDE	AB/CDE	Standard deviation (σ)
Normalize boiling point difference (μ_1)	1	0.145	0.904	0	0.512718
Normalize relative volatility (μ_2)	1	0	1	0.178	0.530962
Normalize Estimated mass load (μ_3)	0.1832	0.5	0.7	0.416	0.213961

The values of R_{ik} are as follows: $R_{12}= 0.965$, $R_{13}= -0.1007$ and $R_{23}= -0.06577$

And then

$C_1 = 0.582167$, $C_2 = 0.584338$ and $C_3 = 0.46354$

And then

$W_1 = 0.357148$, $W_2 = 0.35848$ and $W_3 = 0.284373$

For obtain decision - maker, D, (or the multi-criteria-score of firm), the following table is constructed.

Table 13: Evaluation of decision maker

Solutions	W1. μ_1	W2. μ_2	W3. μ_3	multi-criteria-score (D)	ranking of firm
A/BCD	0.357148	0.35848	0.052097	0.767724	2
AB/CD	0.051786	0	0.142186	0.193973	3
ABC/DE	0.322861	0.35848	0.199061	0.880402	1
ABCD/E	0	0.063809	0.118299	0.182108	4

By comparing the values of multicriteria-score (D) for all the possible split, split ABC/D is chosen for it yield the highest D value that is 1.

The resulting sequence is ABC/D
 Summary of results in **table 14:**

split	ΔT_b	α	EML	μ_1	μ_2	μ_3
A/BC	30.2	2	0.4	1	1	0.6
AB/C	11.4	1.33	0.2	0	0	0.8

Table 15 Summary of result for standard deviation

	A/BC	A/BC	Standard deviation (σ)
Normalize boiling point difference (μ_1)	1	0	0.707107
Normalize relative volatility (μ_2)	1	0	0.707107
Normalize Estimated mass load (μ_3)	0.6	0.8	0.141421

$R_{12} = 1$ $R_{13} = -1$ $R_{23} = -1$

and then

$C_1 = 1.414214$, $C_2 = 1.414214$ and so $C_3 = 0.565685$

and then

$W_1 = 0.416667$, $W_2 = 0.416667$ and $W_3 = 0.204817$

For obtaining decision - maker, D, (or the multi-criteria-score of firm), the following table is constructed:

Table 16: Evaluation of decision maker

Solutions	$W_1.X_1$	$W_2.X_2$	$W_3.X_3$	multi-criteria-score (D)	ranking of firm
A/BC	0.416667	0.416667	0.1	0.833333	1
AB/C	0	0	0.133333	0.133333	2

Comparing the values of multicriteria score (D) for all the possible split, split A/BC is chosen for it yield the highest D value that is 1.

The resulting sequence is **ABC/DE, A/BC, B/C and D/E**
 The total cost of possible separation sequence schemes in table 17

NO.	Separation	Cost*10 ⁶ (\$/yr)
1	ABC/DE,D/E,A/BC,BC	2.087
2	ABC/DE,D/E,AB/C,A/B	2.329
3	AB/CDE,A/B,C/DE,D/E	2.432
4	AB/CDE,A/B,CD/E,C/D	2.758
5	ABCD/E,A/BCD,BC/D,B/C	2.778
6	ABCD/E,ABC/D,A/BC,B/C	2.846
7	ABCD/E,AB/CD,A/B,C/D	2.956
8	ABCD/E,A/BCD,B/CD,C/D	3.056
9	ABCD/E,ABC/D,AB/C,A/B	3.088
10	A/BCDE,BC/DE,B/C,D/E	5.393
11	A/BCDE,BCD/E,BC/D,B/C	5.554
12	A/BCDE,B/CDE,CLDE,D/E	5.692
13	A/BCDE,B/CDE,CD/E,C/D	5.712
14	A/BCDE,BCD/E,B/CD,C/D	5.910

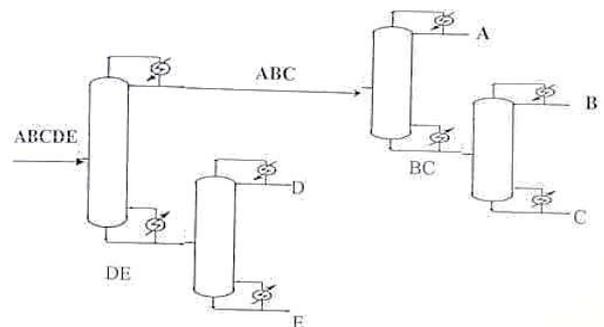


Fig.3 Optimum sequence for five-component mixture separation

The consequence of our approach is comparison with the earlier technique depending on the number of sequences developed (N_{sd}) and the unique search factor (F), which is the ratio of the number of unique subproblems analyzed and the number of unique subproblems. The greater the F value, the lower efficient the search:

Method	N_{sd}	F (%)
HEAVEN(1969)	14	100
RATHORE et al.(1974a,b)	14	100
RODRIGO and SEADER(1975)	11	100
GOMEZ and SEADER (1981)	1	65
NATH and MOTARD(1983)	1	20
NADGIR and LIU (1985)	1	20
GOMEZ and SEADER (1985)	1	20
Y.Y.RAWASH(2002)	1	20

Where N_{sd} is the number of sequence developed

4. CONCLUSION

Multiple criteria decision method has been suggested for synthesis sharp separation sequences by quantification of the three rules. The proposed algorithm method is characterized by its simplicity and can be implemented by hand calculation when applied for problems which had been mentioned earlier in literature yielded optimum solutions which are consistent with the reported values and overcoming the barriers of using heuristic, evolutionary and mathematical programming.

REFERENCE

- [1] Hendry J.E., Rudd D.F and Seader J.D., "Synthesis in the design of chemical process ", *A.I.Ch.E.J.*, 19, PP.1, 1973
- [2] Hlavacek V., " Synthesis in the design of chemical processes", *Comp.&Chem.Eng.*, 2, pp.67, 1978
- [3] Westerberg A.W., "A review of process synthesis ", in "Computer applications to chemical engineering" R.G Squires and G.V.Reklaitis(eds), ACS Symp.Series, 124, Am.Chem.soc., 1980
- [4] Stephanopoulos G., "synthesis of process flow sheet : An adventure in heuristic design or utopia of mathematical programming ", in "Foundations of computer -aided chemical process design " R.H.S.Mah and W.D.Seider(eds), Nat.Sci.Found .New-York, 1981
- [5] Nishida N., Stephanopoulos G. and Westerberg A.W., "A review of process synthesis ", *A.I.Ch.E.J.*, 27, PP.321, 1981
- [6] Umeda T., "Computer-aided process synthesis", *Comp.& Chem.Eng.*, 7, pp.279, 1983
- [7] Westerberg A. W., " The synthesis of distillation-based separation systems", *Comp.&Chem.Eng.*, 9, pp.421, 1985
- [8] Floquet P., Pibouleau L. and Domenech S., "Mathematical programming tools for chemical engineering process design synthesis ", *Chem.Eng.Process.*, 23, pp.99, 1988
- [9] Hendry J.E. and Huges R.R., "Generating separation process flow sheets", *Chem.Eng.Prog.*, 68, pp.71, 1972
- [10] Westerberg A.W. and G.Stephanopoulos (1975), " Studies in process synthesis I: Branch and bound strategy with list techniques for the synthesis of separationschemes", *Chem.Eng.Sci.*, Vol.30, pp.963.
- [11] Rodrigo B.F.R. and J.D.Seader (1975), "Synthesis of separation sequences by ordered branch search ", *A.I.Ch.E. J.* Vol.21, pp.885
- [12] Andreovich M.J. and Westerberg A. W., "A MILP formation for heat-integrated distillation sequence synthesis", *A.I.Ch.E.J.*, 31, pp.1461, 1985
- [13] Floquet P., Pibouleau L. and Domenech S., "Agencement de colonnes de rectification complexes", *Chem.Eng.J.*, 47, PP.119, 1991
- [14] Nath R. And Motard R. L., " Evolutionary synthesis of separation processes", *A.I.Ch.E.J.*, 27, PP.578, 1981
- [15] Lu M.D. and Motard R.L., " Computer-aided total flow sheet synthesis", *Comp.& Chem. Eng.*, 9, pp.43, 1985
- [16] Stephanopoulos G. and Westerberg A.W., " Studies in process synthesis : part II Evolutionary synthesis of optimal process flow sheet", *Chem.Eng.Sci.*, 31, pp.195, 1976
- [17] Seader J.D. and Westerberg A.W., " A combined heuristic and evolutionary strategy for synthesis of simple separation sequence ", *A.I.Ch.E.J.*, 23, PP.951, 1977
- [18] Heaven D.L., " Optimal sequencing of distillation columns in multicomponent fractionation ", M. S. Thesis Univ. of California, Berkeley, 1969
- [19] Powers G.J., " Recognizing patterns in the synthesis of chemical processing systems ", Ph. D. Thesis, Univ. of Wisconsin, Madison, 1971
- [20] Nishimura H. and Hiraizumi Y., " Optimal system pattern for multicomponent distillation systems", *Int.Chem.Eng.*, 11, pp.188, 1971
- [21] Thompson R.W. and King C.J., " Systematic synthesis of separation schemes", *A.I.Ch.J.*, 8, PP.941, 1972
- [22] Rudd D.F., Power G.J. and Siirola J.J., " Process synthesis ", Prentice -Hall, Englewood Cliffs, NJ, 1973
- [23] Niida K., Itoh J., Umeda T. and Ichikawa A., " Some expert system experiments in process engineering", *I.Chem.E.Symp.Series*, 92, pp.529, 1985
- [24] Douglas J.M., " A hierarchical decision procedure for process synthesis ", *A.I.Ch.E.J.*, 31, PP.353, 1985
- [25] Lu M.D. and Motard R.L., " A strategy for the synthesis of separation sequence", *I. Chem. Symp.Series*, 74, pp.141, 1982
- [26] Diakoulaki, D., Mavrotas, G., & Papayannakis, L. (1995). Determining objective weights in multiple criteria problems: The critic method. *Computers & Operations Research*, 22(7), 763-770
- [27] Floudas C.A. and S.H.Anastasiadis (1988), "Synthesis of distillation sequences with several multi-component feed and product streams", *Chem.Eng.Sci.* Vol.43, pp.2407.
- [28] Heaven D.L., " Optimal sequencing of distillation columns in multicomponent fractionation ", M. S. Thesis Univ. of California, Berkeley, 1969